



Astro 500



# *Techniques of Modern Observational Astrophysics*

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University of Wisconsin

# Lecture Outline

## *Spectroscopy from a 3D Perspective*

- ✓ Basics of spectroscopy and spectrographs
- ✓ Fundamental challenges of sampling the data cube
- Approaches and example of available instruments
  - I: Grating-dispersed spectrographs
    - Echelles
    - Bench Spectrograph (WIYN 3.5m)
    - Robert Stobie Spectrograph (SALT 11m)
  - II: Fabry-Perot interferometry
  - III: Spatial heterodyne spectroscopy

# Approaches

## Examples of available instruments

- Interferometry-I: Fabry-Perot imaging
  - the bull's eye: implications for design and use
  - sky stability: calibration design
- Interferometry-II: Spatial-heterodyne spectroscopy
  - low-cost, diffraction-limited high-resolution capability
  - multi-plex disadvantage: implications for design and use

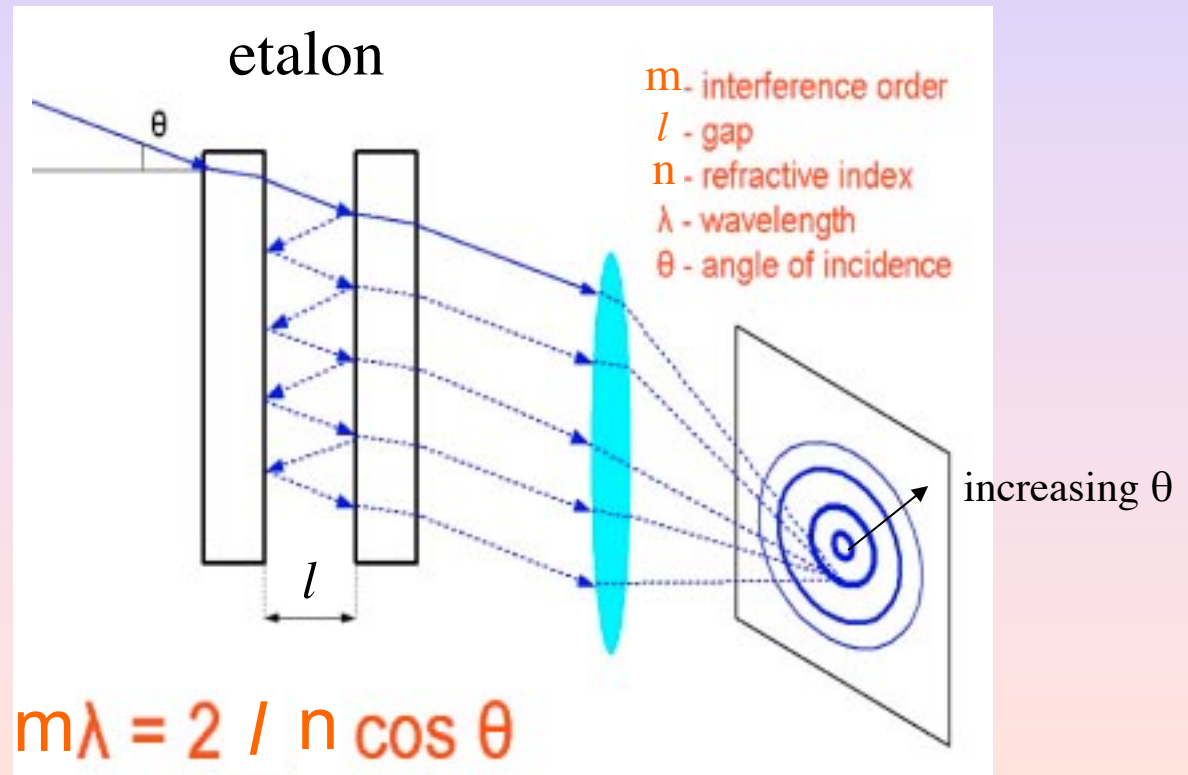
# Fabry-Perot

- A type of interferometer

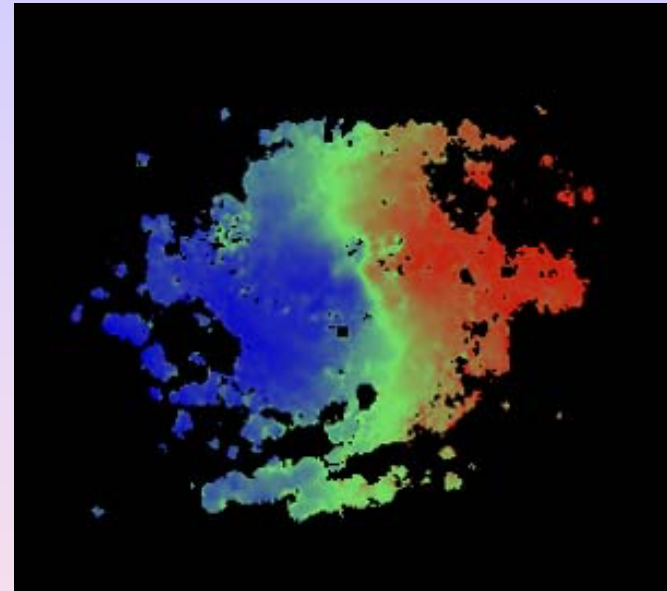
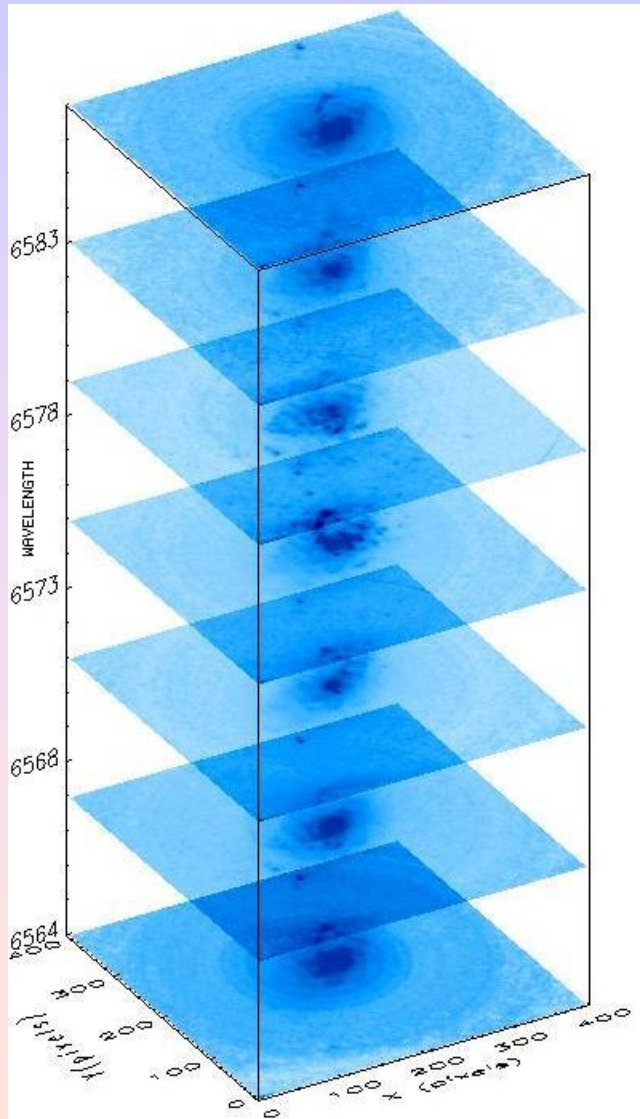
- *Remember:* angles in a collimated beam correspond to different field points at a focus.

- So what happens if the etalon is not in a collimated beam?

What about the apex angle of the diverging/converging beams?



# F-P data cube for an imaging system

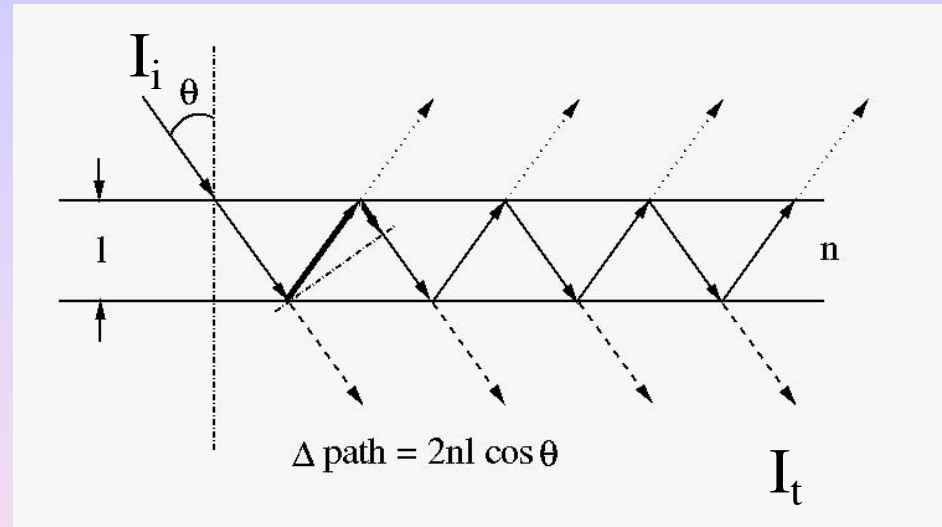


Color-coded velocity map

But in reality each “snap-shot” with etalon-gap  $d$  is only monochromatic at a given field point from the optical axis, i.e., the observed data-cube is curved and has to be wavelength-rectified.

# Interferometry-I: Fabry-Perot imaging Basics

- **Etalons** (flat glass plates) are spaced by some distance  $l$ , filled with gas of refractive index  $n$ , and coated to have high reflectivity.
- Light incident at some angle,  $\theta$ , produces internal reflections, with transmission when  $\Delta\text{path}$  yields positive interference.



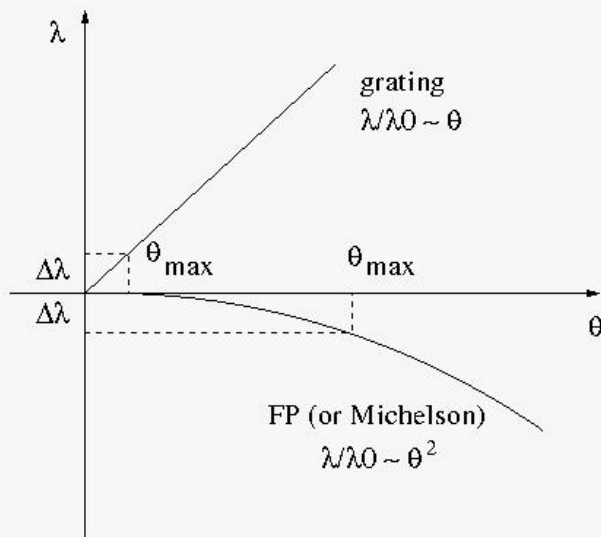
- $I_t/I_i$  given by Airy function with peaks  $I_t=I_i$  when  $\Delta\text{path} = m\lambda$ , or  

$$\lambda_\theta = (2nl/m) \cos \theta$$

$$= \lambda_0 \cos \theta$$
- Compare to grating equation:  

$$\lambda = (2 \sigma/m) \sin \theta \quad (\text{Littrow})$$

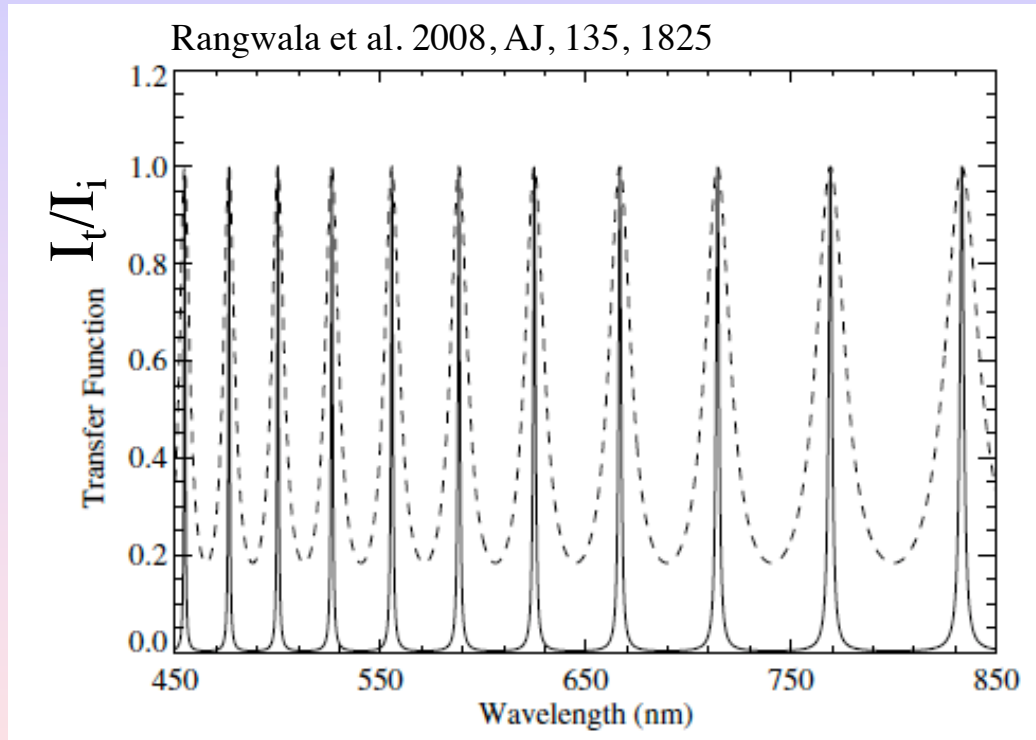
➤ *FP is field-widened for same spectral resolution*





# Interferometry-I: Fabry-Perot imaging

## Transmission



**Airy function transmission profiles** with  $l = 5 \mu\text{m}$  and coatings with reflectivity  $\mathcal{R}$  of 0.8 (solid) and 0.45 (dashed)

$$I_t = I_i \frac{T^2}{(1-R)^2} \frac{1}{1 + F \sin^2(\Delta/2)}$$

$$\Delta = 4\pi l \cos \theta / \lambda$$

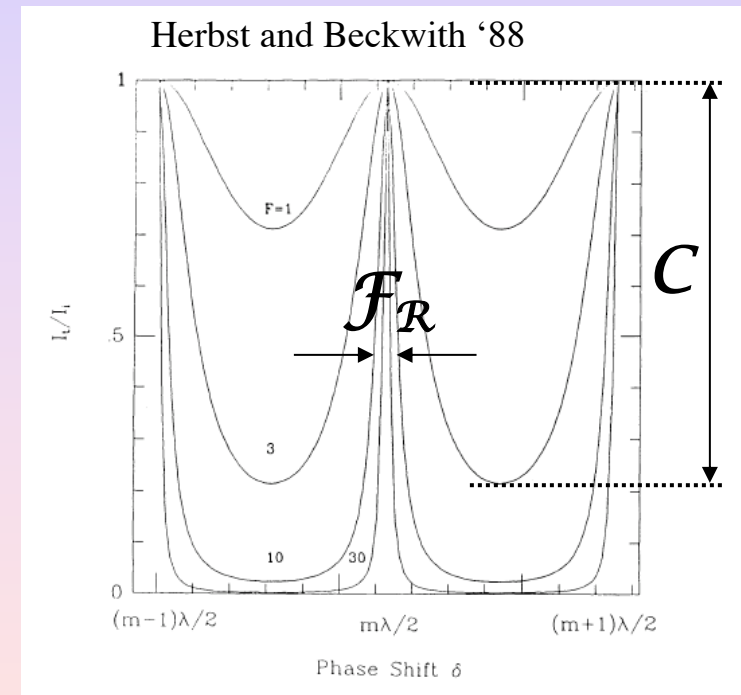
$$\mathcal{F} = 4\mathcal{R} (1-\mathcal{R})^2$$

↑  
*Finesse (bien sur)*  
(here just the reflective finesse)

# Interferometry-I: Fabry-Perot imaging

## Useful relations

- **Tune** gap ( $l$ ) or pressure (index  $n$ ) to control/scan central wavelength
  - $\lambda_0 = (2nl/m) \cos \theta$
- **Q** = free spectral range
  - $= \lambda^2 / 2l \sim 1 / 2n l \cos \theta$
  - order blocking filters are needed
- **R** =  $\lambda / d\lambda = 2l \mathcal{F}_R / \lambda = m \mathcal{F}_R$ 
  - ↖ *spectral resolution*
  - ↗ *reflectivity*
- $\mathcal{F}_R$  = reflective finesse =  $\pi \mathcal{R}^{1/2} / (1 - \mathcal{R})$ 
  - ~ number of back/forth reflections;
  - typical values of 20 to 30 in astro. apps.
  - $\mathcal{R} \sim$  total path difference divided by  $\lambda$ .
  - High resolution requires:  
large gaps and high finesse.
- **C = Contrast** =  $I_{\max} / I_{\min} = (1 + \mathcal{R})^2 / (1 - \mathcal{R})^2 = 1 + 4(\mathcal{F}_R / \pi)^2$





# Interferometry-I: Fabry-Perot imaging

## Bull's eye (Jaquinot spot) and rings

- **The bull's eye:**

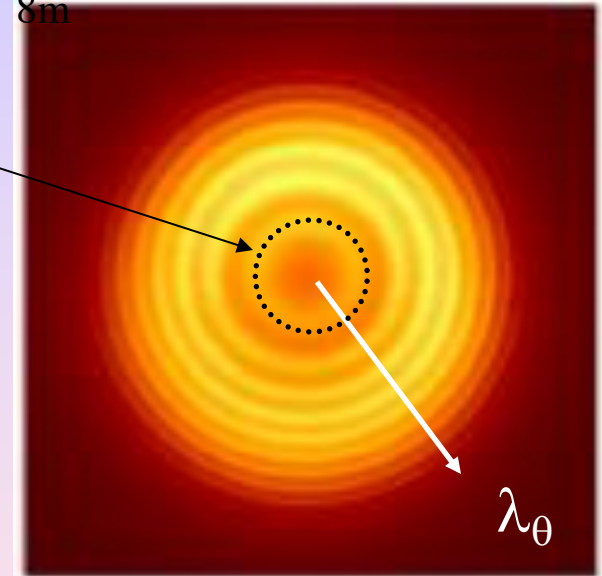
- What is  $\theta$  so that  $\lambda_0/|\lambda_0-\lambda_\theta| < R$  ?
- $\theta_{\max} = (2/R)^{1/2}$
- This quantity is *independent* of the telescope, and is a property of the etalon.

Where does this come from?

What's the angle of the nth ring?

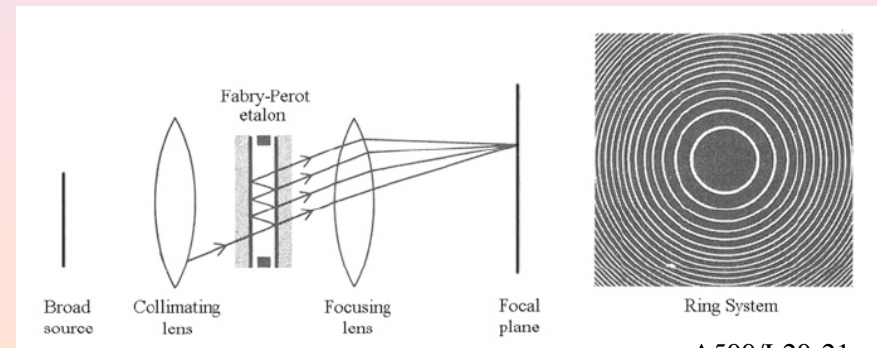
How does the ring area (within the resolution element) change with n?

Hartung et al.'04 NACO, VLT  
8m



- Couple to a telescope to modify angular resolution:

- $A\Omega$  is conserved
- $\alpha = \theta D_e / D_T$ 
  - o  $\alpha$  = angle on the sky
  - o  $\theta$  = angle on the etalon
  - o  $D_e$  = etalon diameter
  - o  $D_T$  = telescope diameter



# Interferometry-I: Fabry-Perot imaging

## Finesse

*Finesse:*  
(mais oui)

$$\frac{1}{\mathcal{F}^2} = \frac{1}{\mathcal{F}_R^2} + \frac{1}{\mathcal{F}_D^2}.$$

Reflective finesse

Defect finesse:

See: Atherton et al. 1981  
Opt. Eng. 806, 20

$$\frac{1}{\mathcal{F}_D^2} = \frac{1}{\mathcal{F}_{Dc}^2} + \frac{1}{\mathcal{F}_{Dr}^2} + \frac{1}{\mathcal{F}_{Dp}^2}.$$

$$\mathcal{F}_{Dc} = \frac{\lambda}{2\delta t_c}$$

Plate curvature

$$\mathcal{F}_{Dr} = \frac{\lambda}{4.7\delta t_r}$$

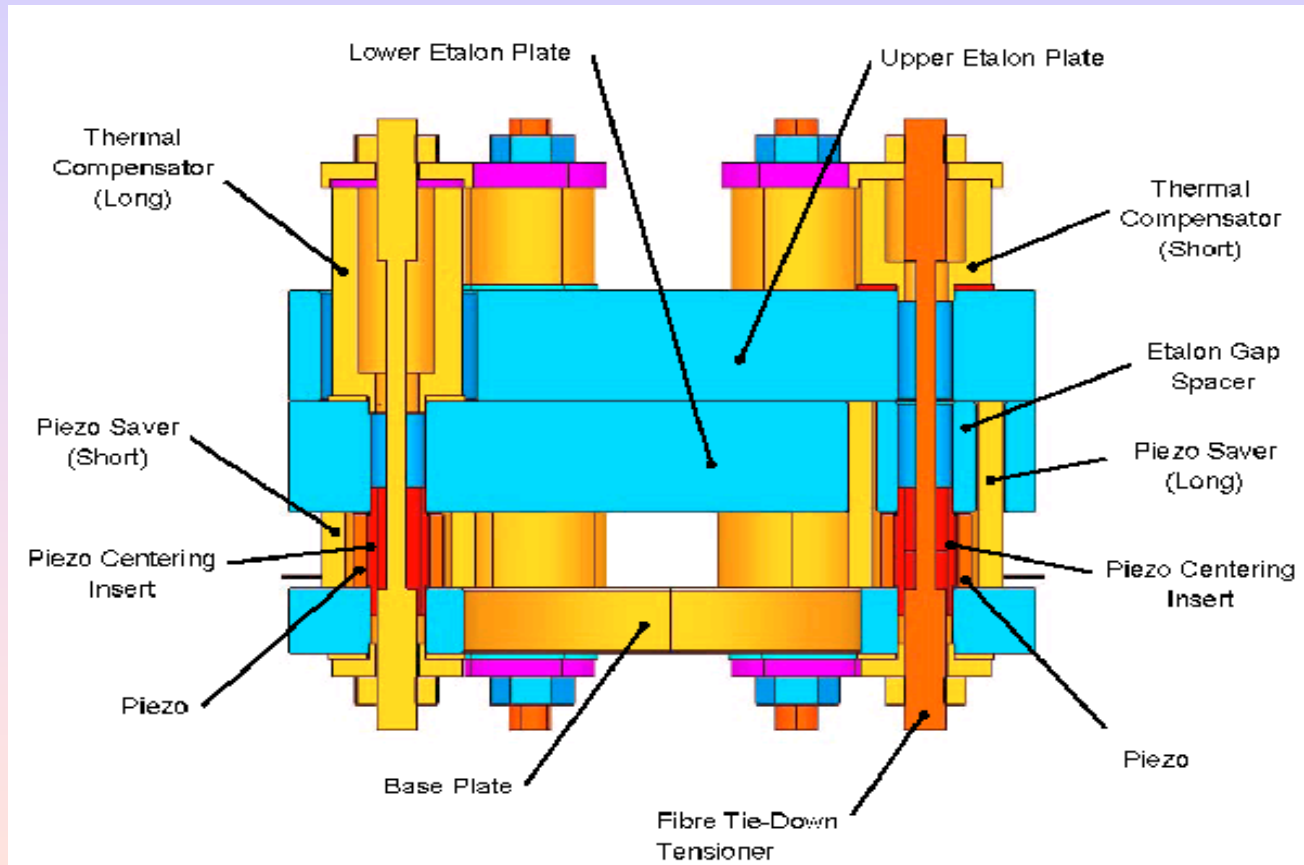
Surface irregularities/roughness

$$\mathcal{F}_{Dp} = \frac{\lambda}{\sqrt{3}\delta t_p}$$

Departure from parallelism

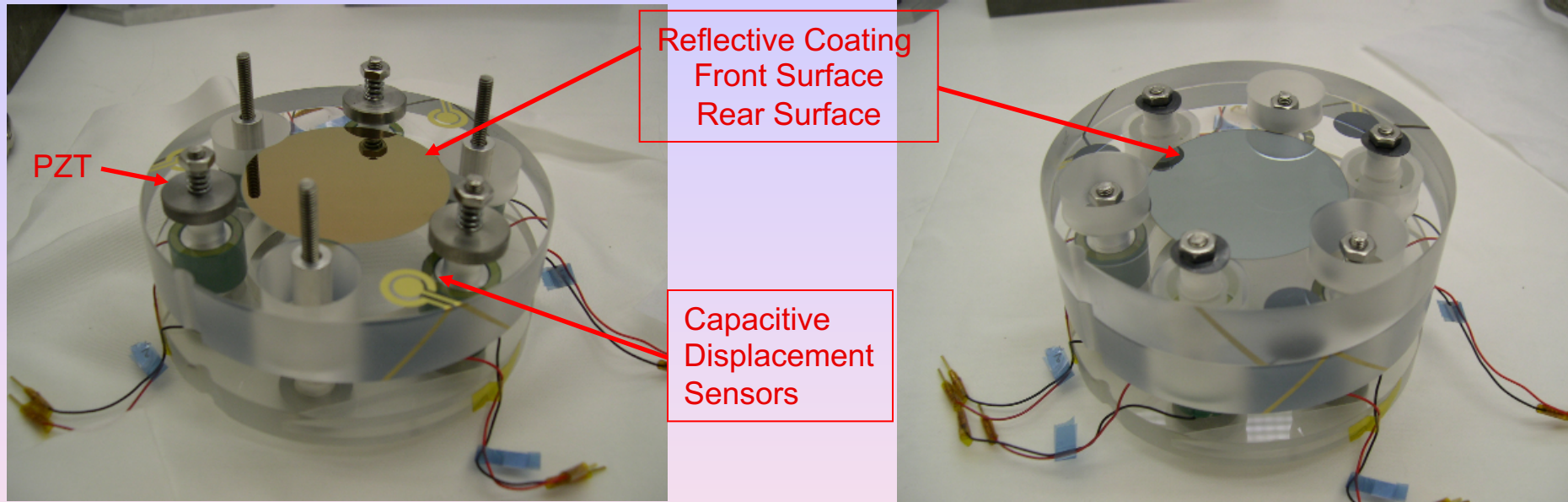
# An Example: JWST Etalon Design

[Courtesy: Bob Abraham and the F2T2 Team]



# Etalon Prototype

[Courtesy: Bob Abraham and the F2T2 Team]



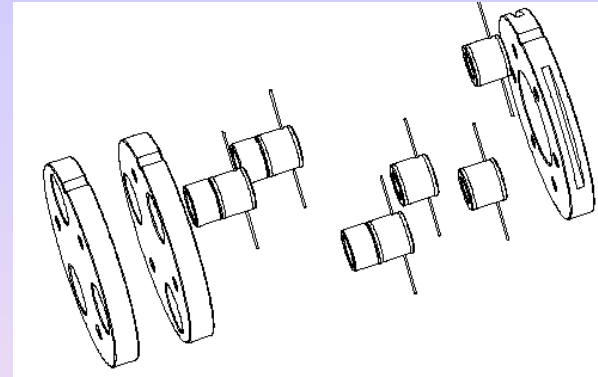
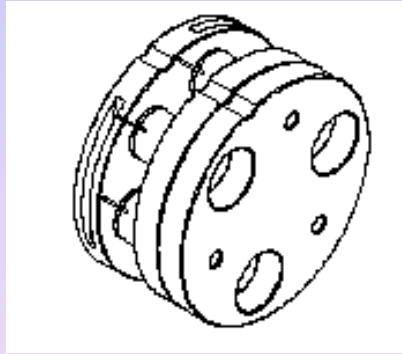
Bottom Plate & Mounting Ring

Completed Etalon

- The etalon consists of two 20 mm thick  $\text{SiO}_2$  plates with the reflective coating applied in the central  $\sim 50$  mm
- There are three piezo-electric transducers supporting the bottom plate and three PZTs + spacers supporting the top plate
- Capacitive displacement sensors are used to control the spacing of the etalon plates

# JWST Etalon

## Basic Design Features



- Etalon plates surface figure better than 11 nm before coating (32 nm after).
  - Meets optical requirement of finesse.
  - Optical materials are silicon for LW etalon and silica for SW.
- 7.5  $\mu\text{m}$  nominal gap parallel over clear aperture.
  - Translates to a 4.5  $\mu\text{m}$  gap between the coatings, because of coating thickness.
  - Nominal gap is set by precise manufacture of spacers made of plate material.
- Gap to be stepped using piezoelectric actuators.
  - Six actuators in total, three for the top plate, three for the bottom.
  - Larger of two available sizes selected for higher bearing area.
- Gap spacing feedback provided by capacitive displacement sensors.

# JWST TFI Etalon Requirements

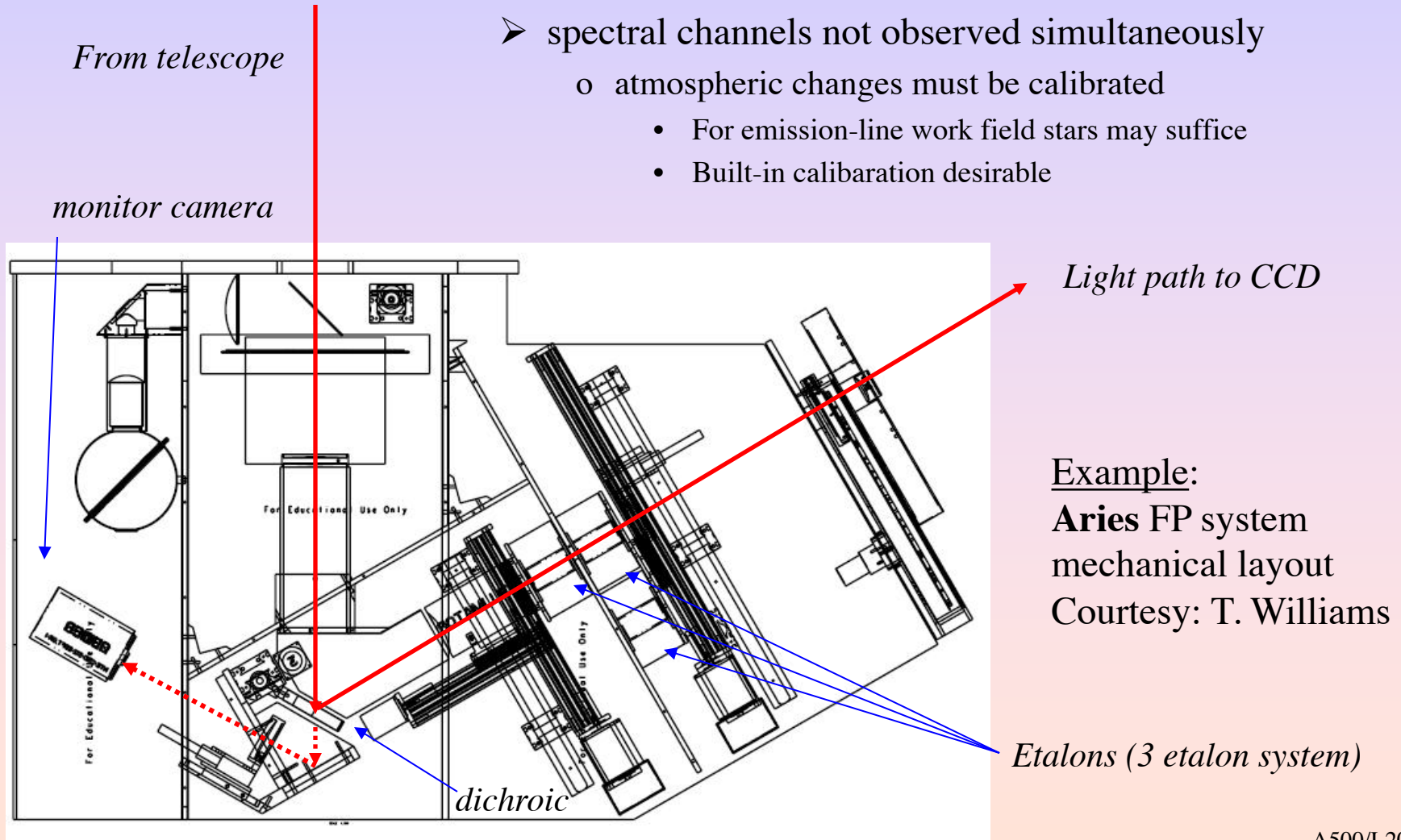
Parameter	Shortwave Etalon	Longwave Etalon	Notes
Wavelength Range	1.2 to 2.1 $\mu\text{m}$	2.0 to 4.8 $\mu\text{m}$	Wavelength ranges are not finalized, transition wavelength may be lower
Spectral Resolution	$R > 80$		Etalon intrinsic resolution higher than requirement on FGS-TF channels.
Clear Aperture	56 mm		Pupil size $\sim 40$ mm. Set by etalon location in optical path
Finesse	$\sim 30$		Compromise between fabrication challenges & minimizing # of blockers
Surface Figure (P-V)	$< 30$ nm	$< 60$ nm	Coated etalon surface figure must support reflectance finesse.
Transmittance	$> 75\%$		Will be set primarily by achieved surface figure.
Contrast	$> 100$		Peak transmittance divided by minimum between spectral peaks
Passband Shift with FOV	$< 5\%$		Ideal air spaced etalon has $< 1.2\%$ , typical designs have $< 2.5\%$
Number of Blocking Filters	$< 6$	$< 6$	Goal is to minimize filter wheel size and simplify operations.

- The free spectral range is maximized by using a low order: small gap spacing
- A finesse of  $\sim 30$  and a spectral resolution of  $R \sim 100$  suggest operating in 3<sup>rd</sup> order.

# Interferometry-I: Fabry-Perot imaging

## Ground-based instruments

- Sky stability:
  - spectral channels not observed simultaneously
    - atmospheric changes must be calibrated
      - For emission-line work field stars may suffice
      - Built-in calibration desirable



Example:  
**Aries** FP system  
mechanical layout  
Courtesy: T. Williams



# Interferometry-I: Fabry-Perot imaging

## Ground-based instruments: RSS

- RSS, SALT 9.2m
  - Imaging FP
  - 150 mm etalons
  - 9200 mm telescope
  - 8 arcmin FoV, 0.2 arcsec sampling
  - $R = 300$  to 9000 in 4 modes
  - 430-860 nm

3 Etalons:  $l = 5\text{-}11, 27, \text{ and } 135 \mu\text{m}$

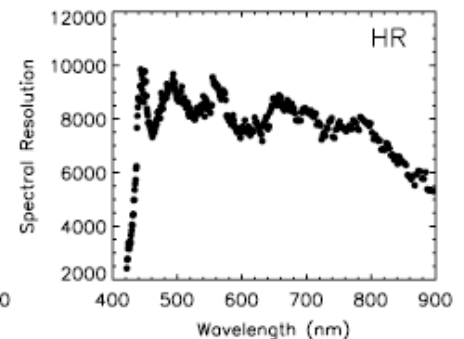
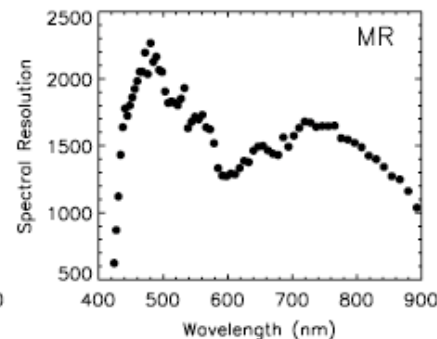
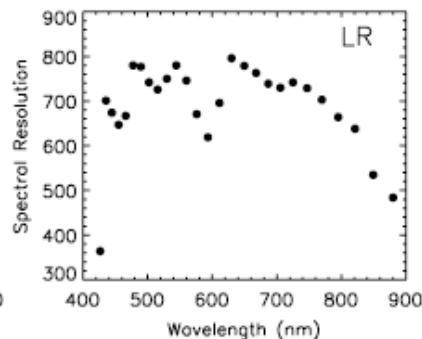
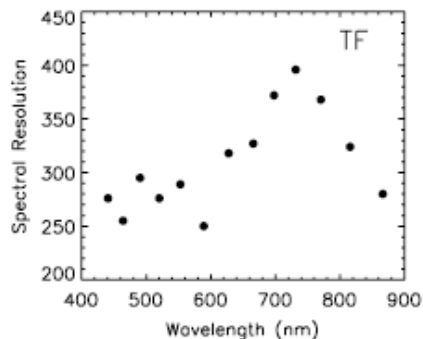
$$\begin{aligned}\mathcal{F}_D &\sim 50 \\ \mathcal{F}_R &= 30 \\ \longrightarrow \mathcal{F} &\sim 25\end{aligned}$$

SG etalon  $l=5\text{-}7 \mu\text{m}$

SG etalon  $l=9\text{-}11 \mu\text{m}$

SG+  
MG etalon  $l=22\text{-}28 \mu\text{m}$

SG+  
LG etalon  $l=130\text{-}136 \mu\text{m}$

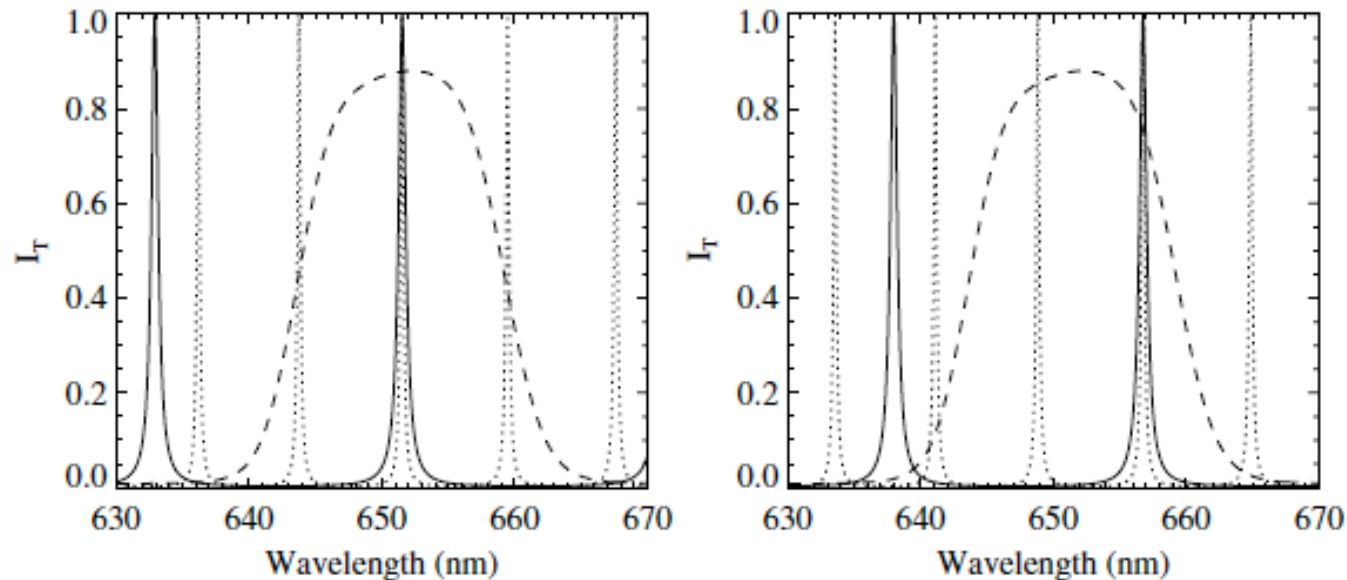


Rangwala et al. 2008, AJ, 135, 1825

# Interferometry-I: Fabry-Perot imaging

## Ground-based instruments: RSS

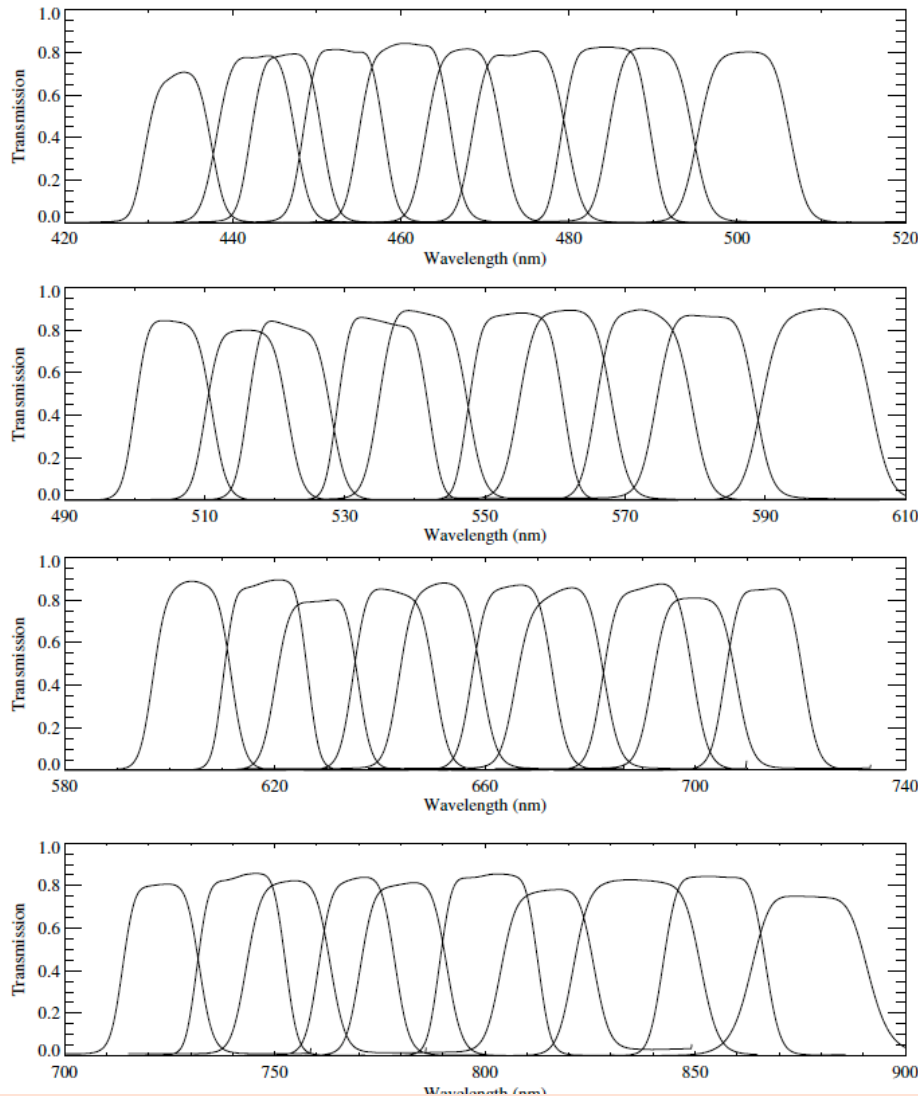
### Dual-etalon + filter order blocking scheme



Order selection with interference filter and dual etalons. Solid curve: SG etalon; dashed curve: filter; dotted curve: MG etalon.

# Interferometry-I: Fabry-Perot imaging

## Ground-based instruments: RSS

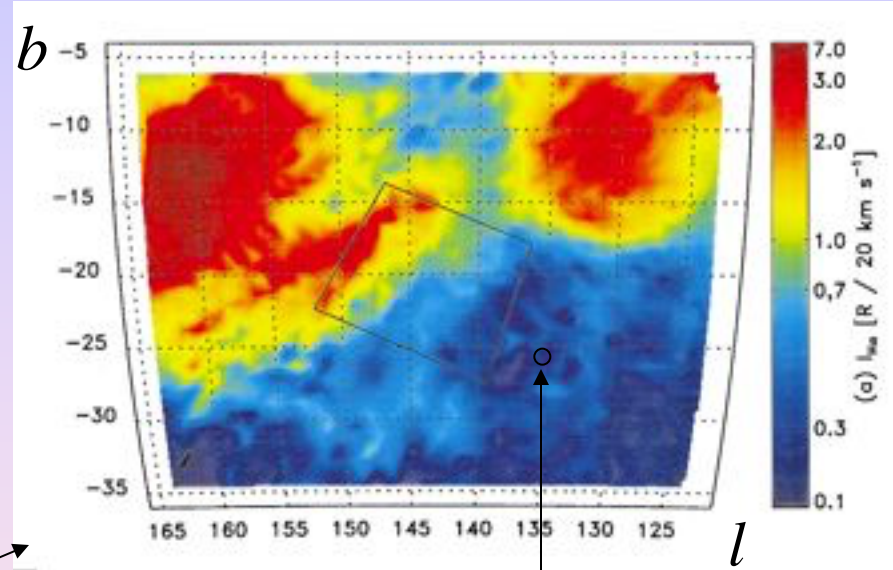


Suite of NB filters for FP ...  
...but remember you can use  
them for imaging or for  
filtered spectroscopy (MMS  
mode)

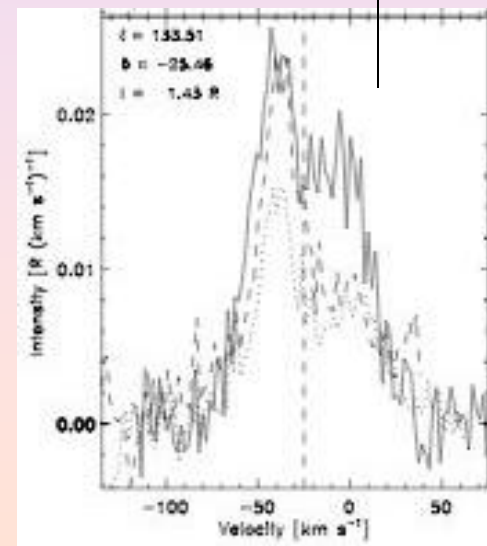
# Interferometry-I: Fabry-Perot imaging

## Ground-based instruments

- Two extremes:
- RSS, SALT 9.2m
  - **Imaging** FP
  - 150 mm etalons
  - 9200 mm telescope
  - 8 arcmin FoV, 0.2 arcsec sampling
  - $R = 300-9000$



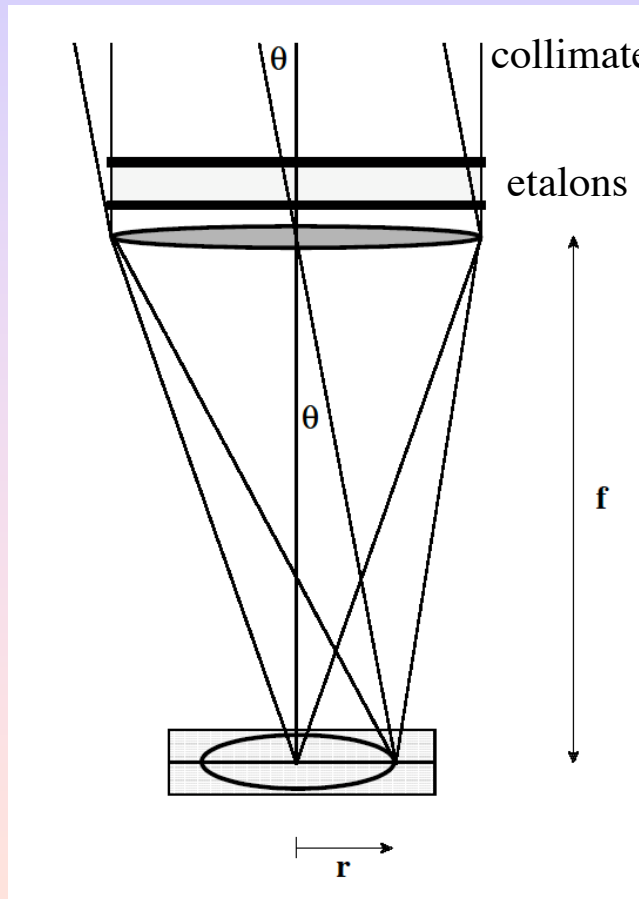
- WHAM
  - Wisconsin H $\alpha$  Mapper*
  - **Non-imaging** FP
  - 150 mm etalons
  - 600 mm telescope
  - 1 deg FoV and sampling
  - $R = 25000$



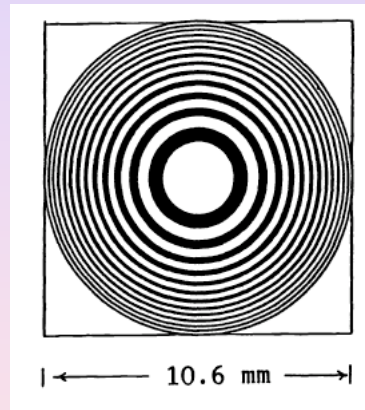
# Interferometry-I: Fabry-Perot imaging

## Ground-based instruments: WHAM

- An imaging FP

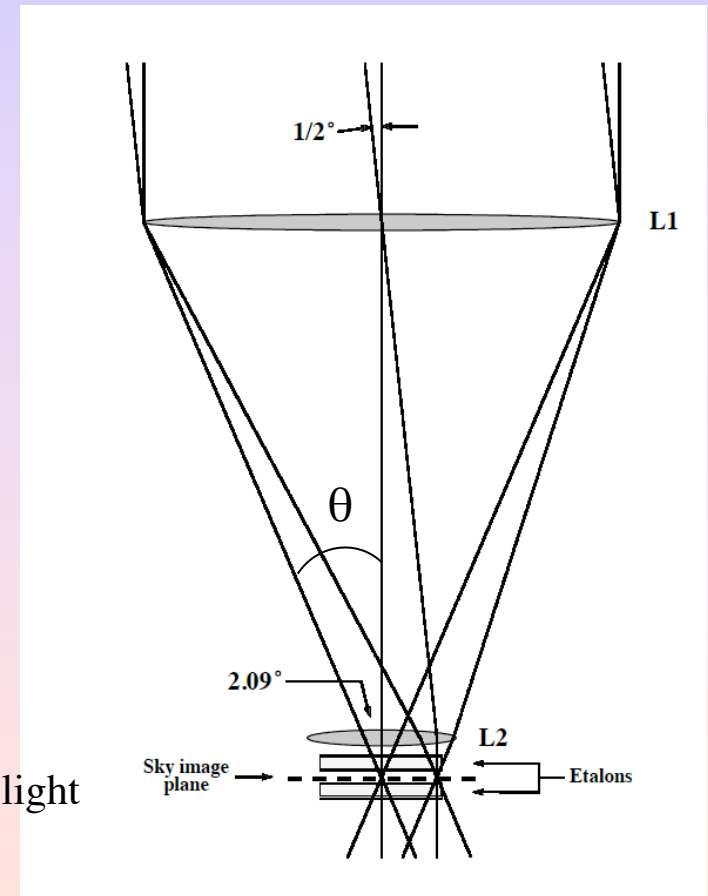


At the detector:



converging light

- A non-imaging FP



What determines the number of rings?

# Interferometry-I: Fabry-Perot imaging

## Bull's eye (Jaquinot spot) and rings - *revisitus*

- **The bull's eye:**

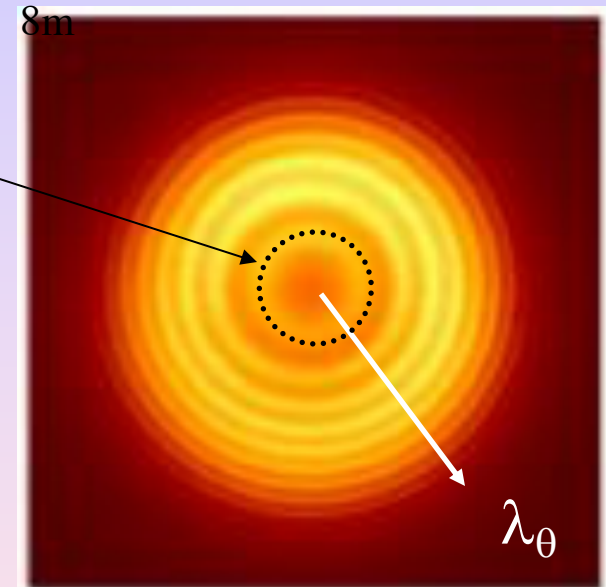
- What  $\theta$  so that  $\lambda_0/|\lambda_0-\lambda_\theta| < R$  ?
- $\theta_{\max} = (2/R)^{1/2}$
- This quantity is *independent* of the telescope, and is a property of the etalon.

Where does this come from?

What's the angle of the nth ring?

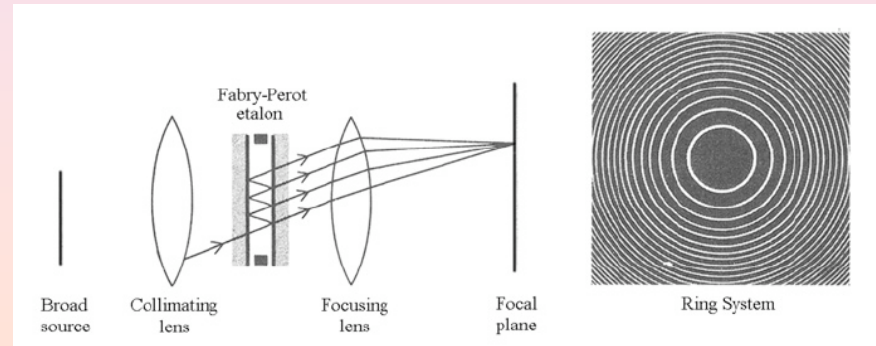
How does the ring area (within the resolution element) change with n?

Hartung et al.'04 NACO, VLT

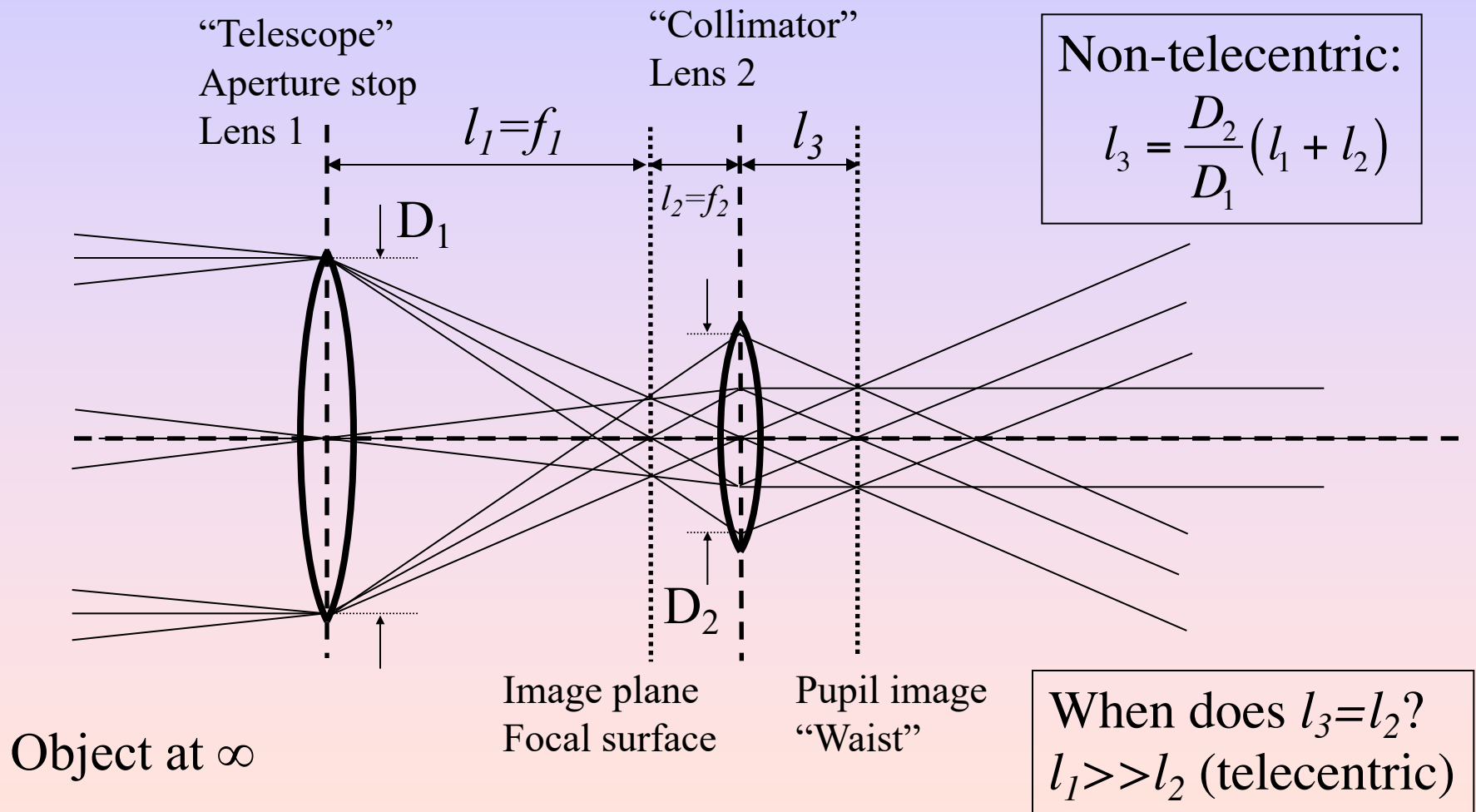


- Couple to a telescope to modify angular resolution:

- $A\Omega$  is conserved
- $\alpha = \theta D_e / D_T$ 
  - o  $\alpha$  = angle on the sky
  - o  $\theta$  = angle on the etalon
  - o  $D_e$  = etalon diameter
  - o  $D_T$  = telescope diameter

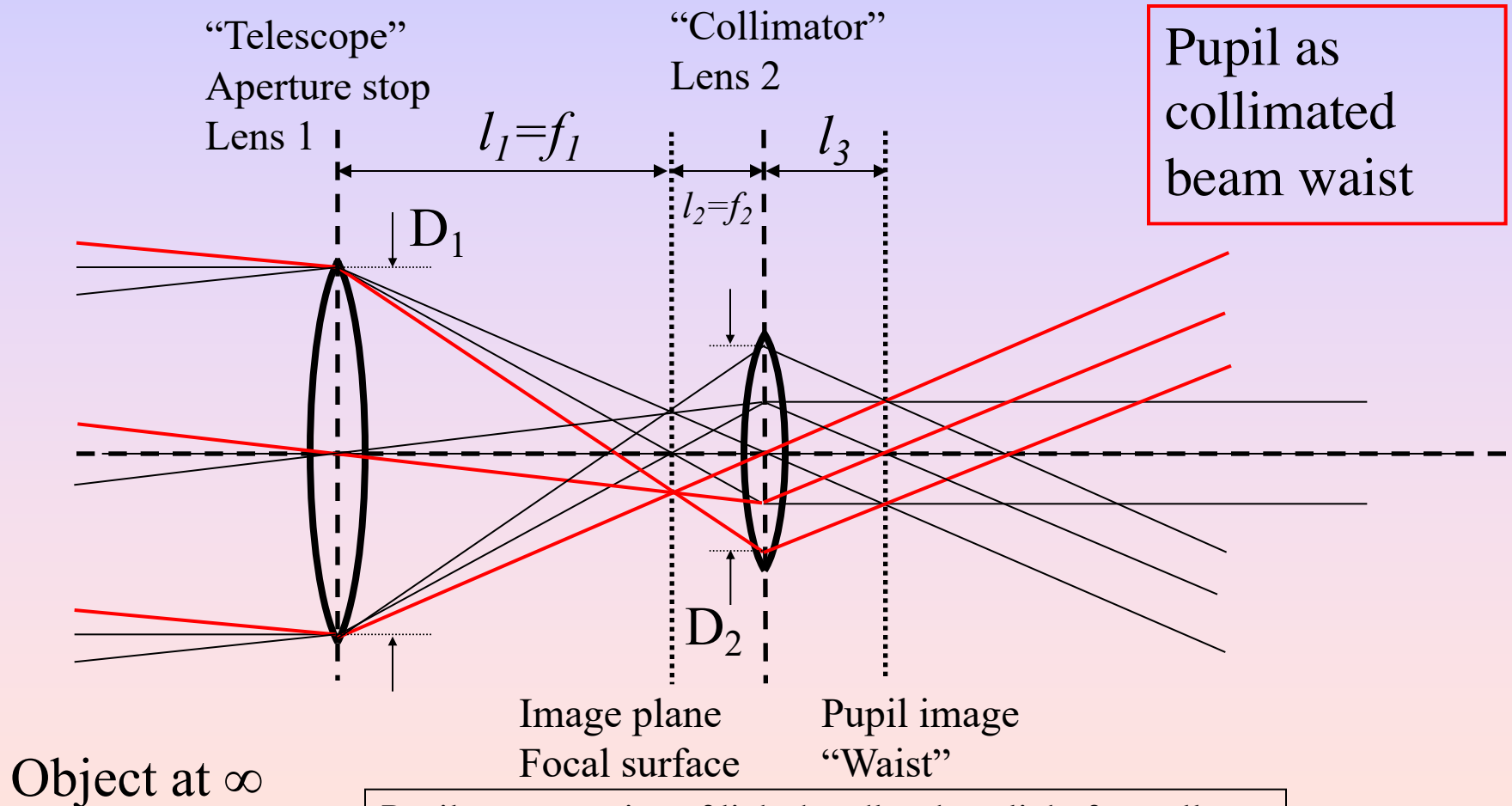


# Objects, Images, Pupils



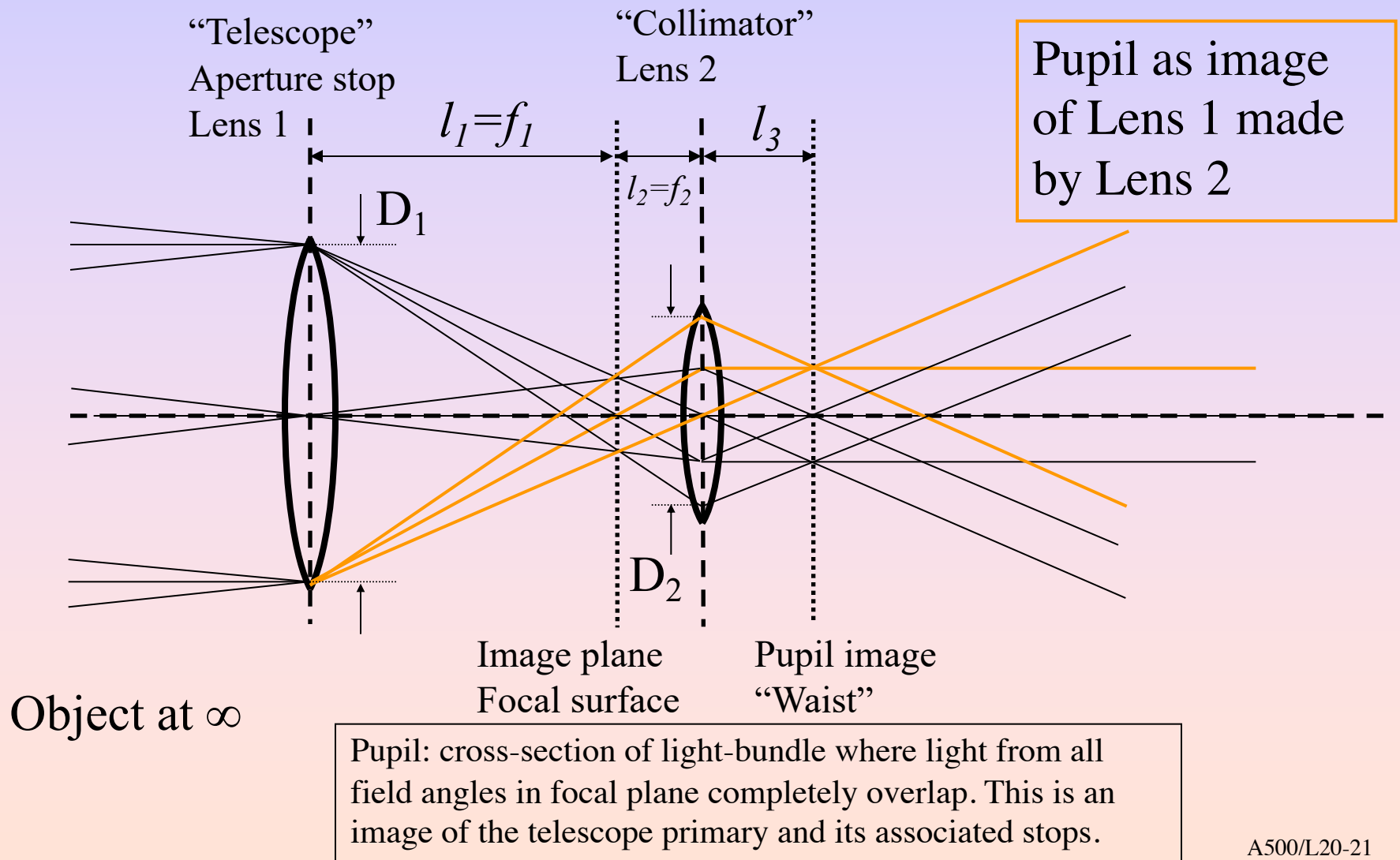


# Objects, Images, Pupils



Pupil: cross-section of light-bundle where light from all field angles in focal plane completely overlap. This is an image of the telescope primary and its associated stops.

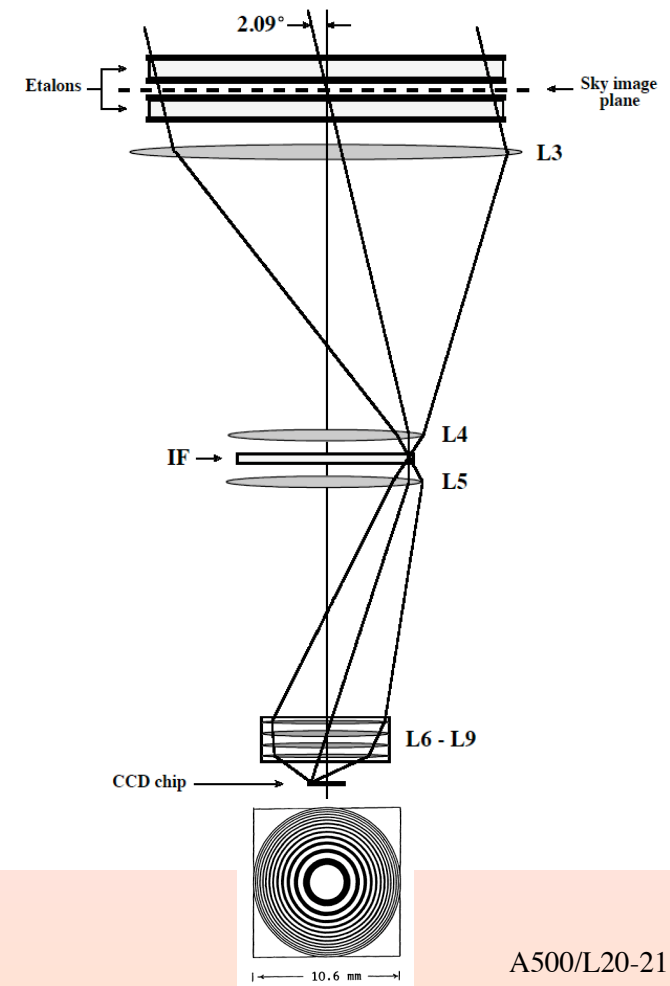
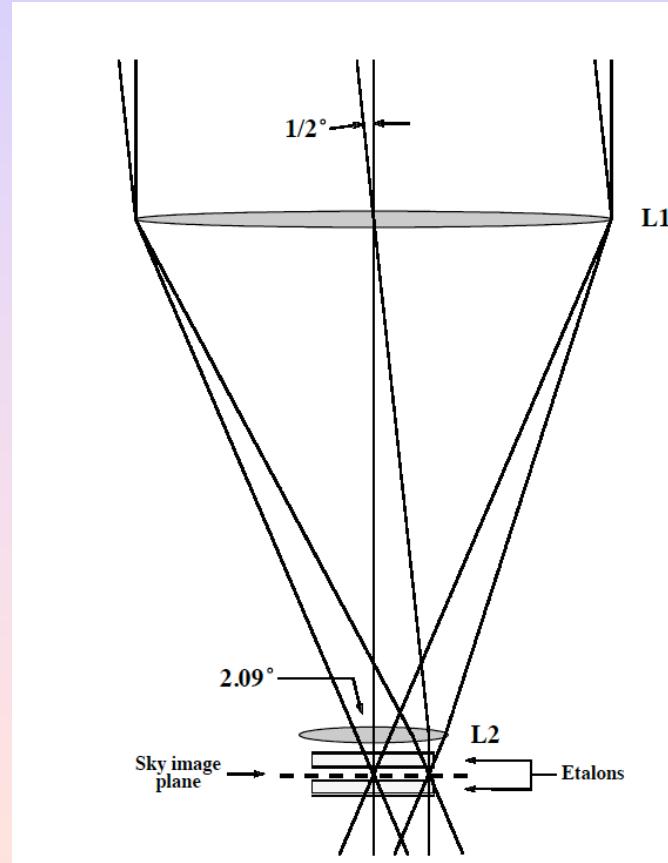
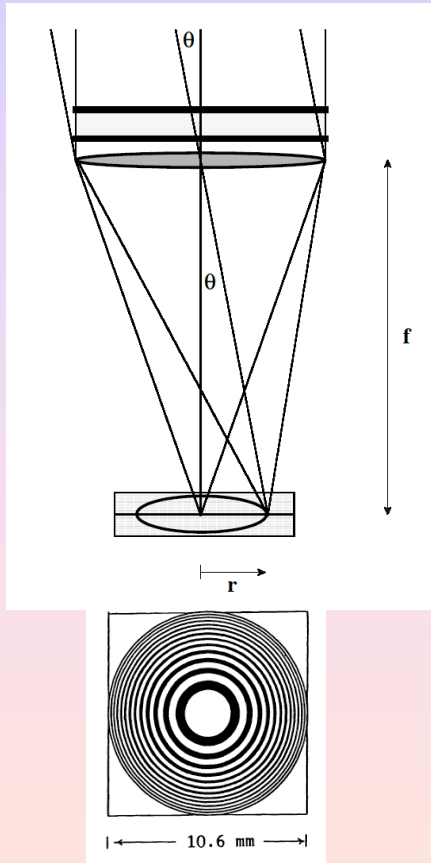
# Objects, Images, Pupils



# Interferometry-I: Fabry-Perot imaging

## Ground-based instruments: WHAM

- An imaging FP
- A non-imaging FP



# Interferometry-I: Fabry-Perot imaging

## Fabry-Perot instruments - summary list

- Existing optical instruments
    - GHASP, HPO 1.9m
    - RFPI, CTIO 4m
    - RSS, SALT 9.2m
  - Future optical instruments
    - OSIRIS, GTC 10.4m
  - Existing infrared instruments
    - NACO, VLT 8,
  - Future NIR instruments
    - FGS-TF, JWST 6.5m
- ← Never made it

*This list is incomplete*

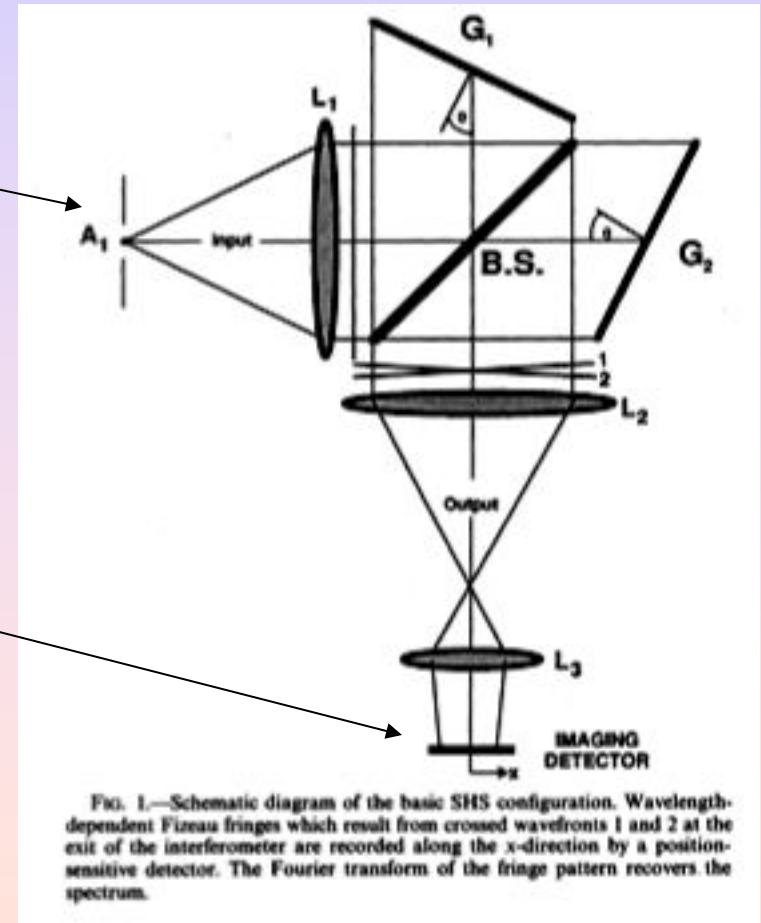
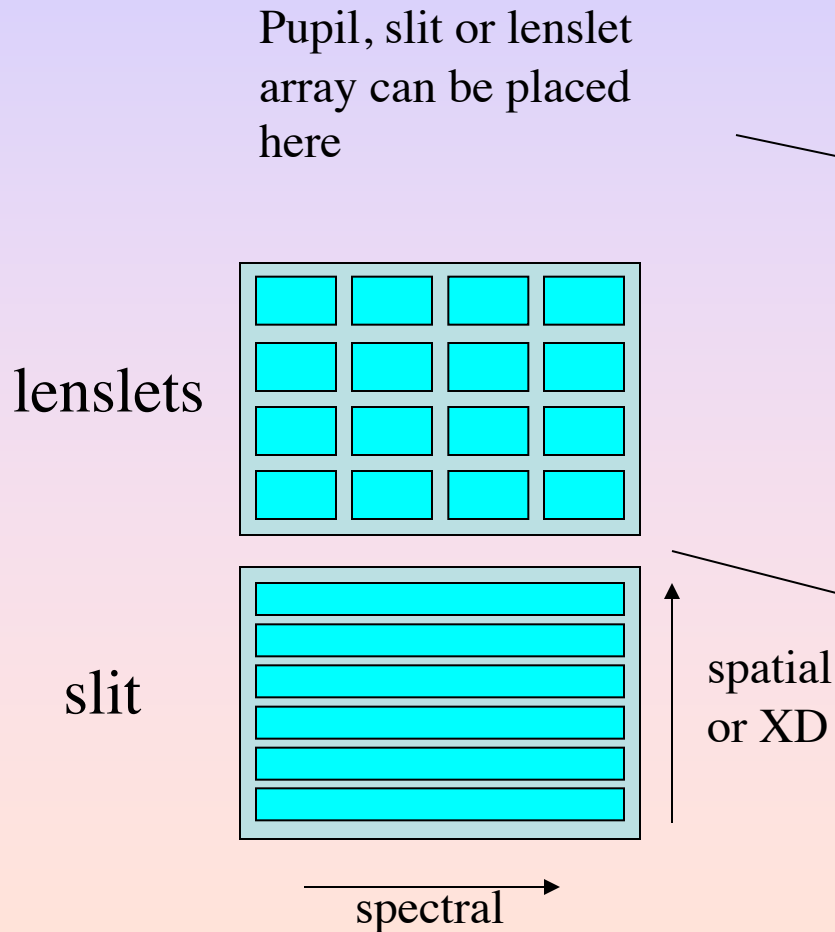
# Interferometry-II:

## Spatial-heterodyne spectroscopy

- What is an SHS?
  - A Michelson interferometer with gratings replacing the mirrors
  - Principles of operation
  - Advantage over Michelson: no stepping required
  - Field widening-possible
  - Long-slit and lenslet feeds possible
  - Non-lossy geometries possible
  - Cross-dispersion possible (tilt one grating), but the same fundamental limits apply concerning 3D information formatted into a 2D detector!
- low-cost, diffraction-limited high-resolution capability
- multiplex disadvantage: implications for design and use

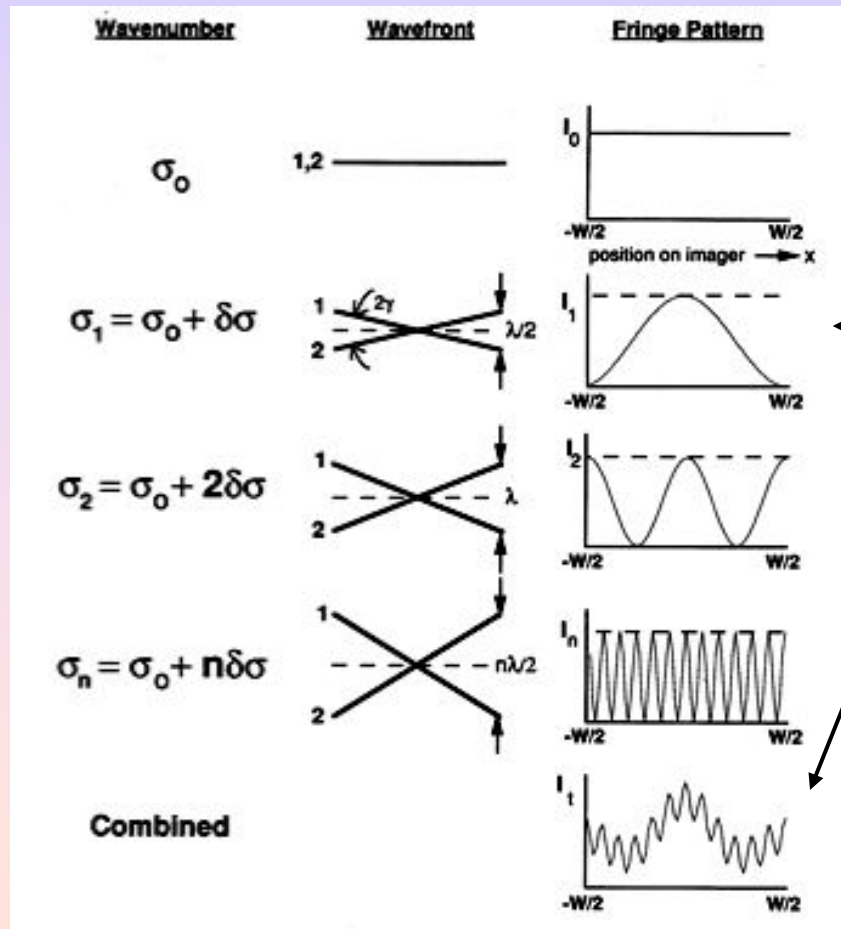
# Interferometry-II: Spatial-heterodyne spectroscopy

## Instrument lay out



# Interferometry-II: Spatial-heterodyne spectroscopy

## Principles of operation



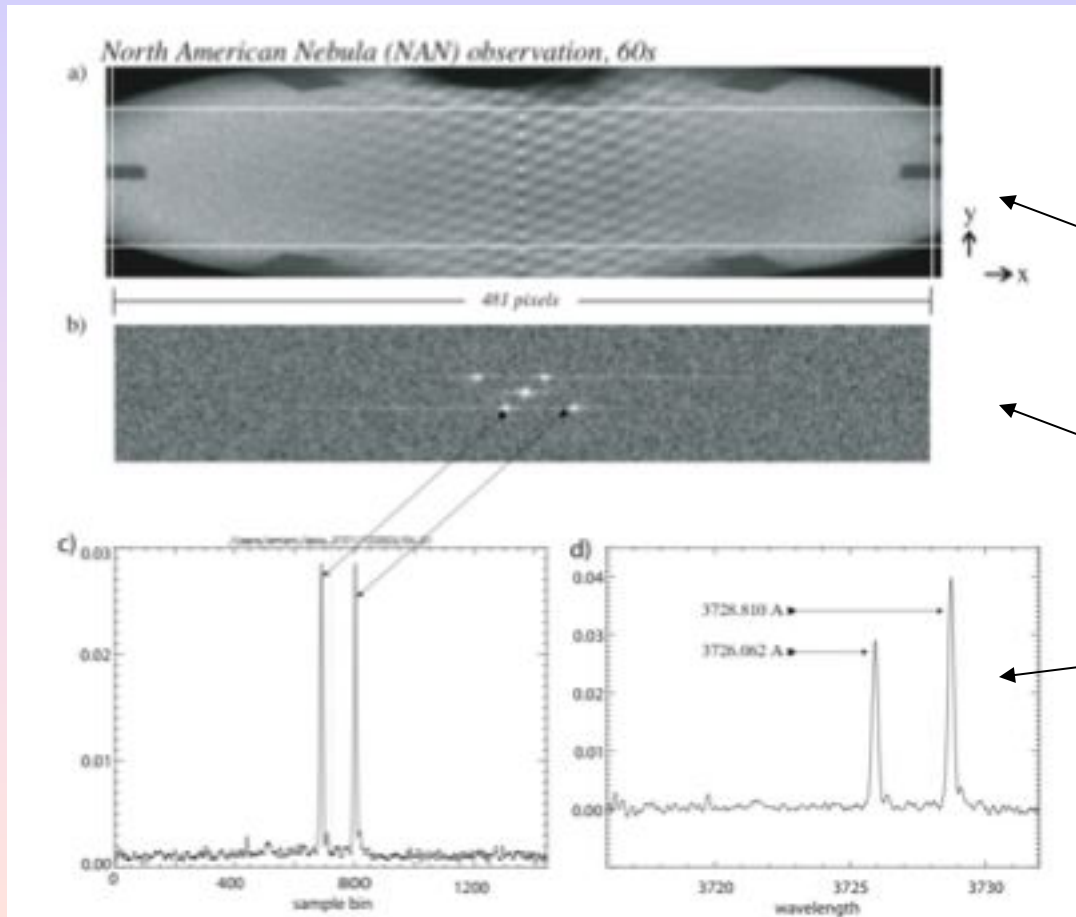
- Gratings diffract light at wavelength-dependent angles.
- Wavefronts produce interference patterns with frequencies set by wavelength.

- *Resolution* is set by the grating aperture diameter.
- *Bandwidth* is set by the length of the detector (how many frequencies can be sampled depends on the number of pixels)

The signal is heterodyned about the frequency of the central wavelength.



# Interferometry-II: Spatial-heterodyne spectroscopy



PBO SHS data

courtesy Harlander, Roesler,  
and Reynolds

OII interferogram  
with cross-dispersion  
via grating tilt

FT power spectrum

Wavelength calibrated,  
filter-corrected [OII]  
spectrum

Resulting [OII] spectrum

# Interferometry-II: Spatial-heterodyne spectroscopy

## Field-widened Michelson

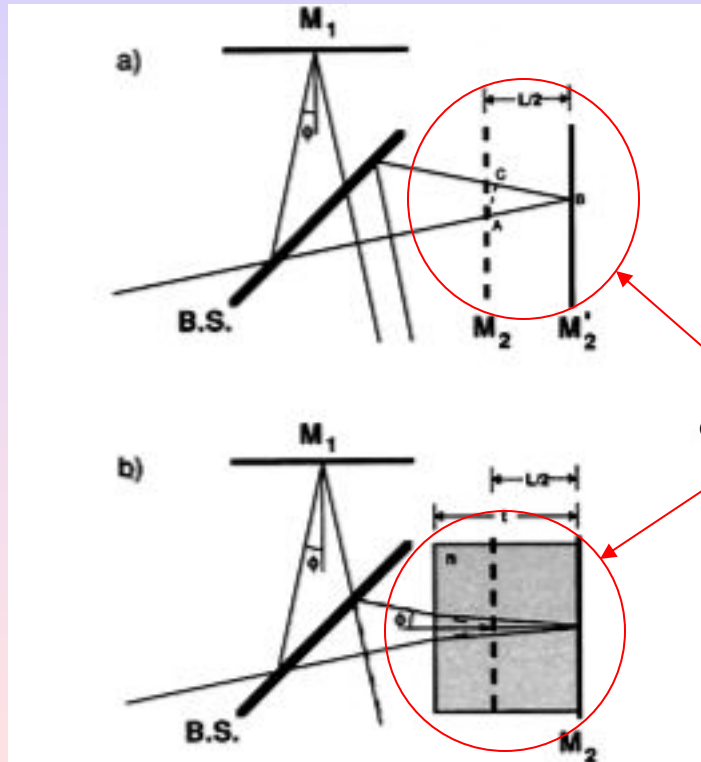


FIG. 3.—(a) Off-axis properties of a Michelson interferometer. When mirror at  $M_2$  is moved to position  $M'_2$ , the path difference in the system becomes a function of off-axis angle  $\phi$ . If the path difference for axial rays is  $L$ , as shown in the figure, then the off-axis path difference, denoted in the figure by  $AB + BC$ , is  $L \cos \phi$ . (b) Field-widened Michelson interferometer. When a material with refractive index  $n$  and thickness  $t$  is placed in front of the displaced mirror  $M'_2$ , the quadratic dependence on path difference with off-axis angle is eliminated. The thickness of the material is chosen so the geometric images of  $M_1$  and  $M_2$  appear coincident.

compare

## Field-widened SHS

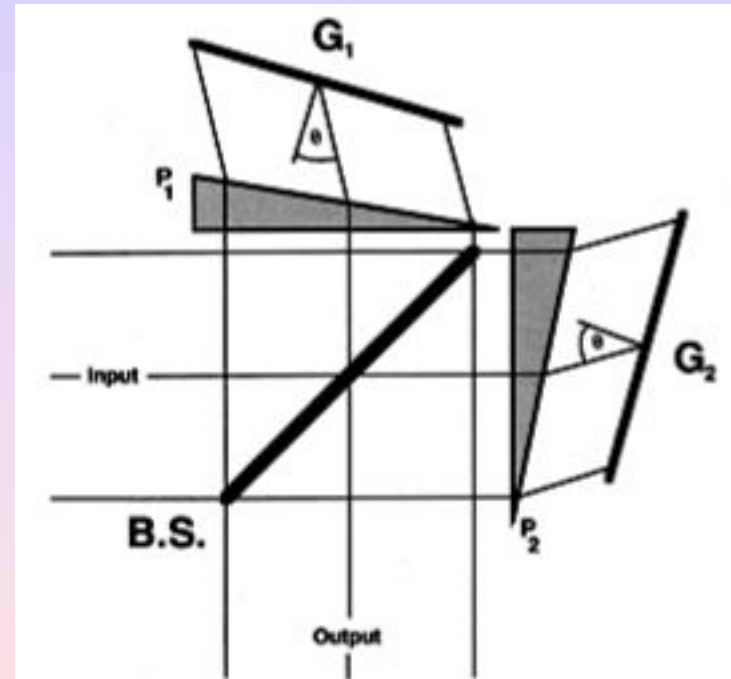
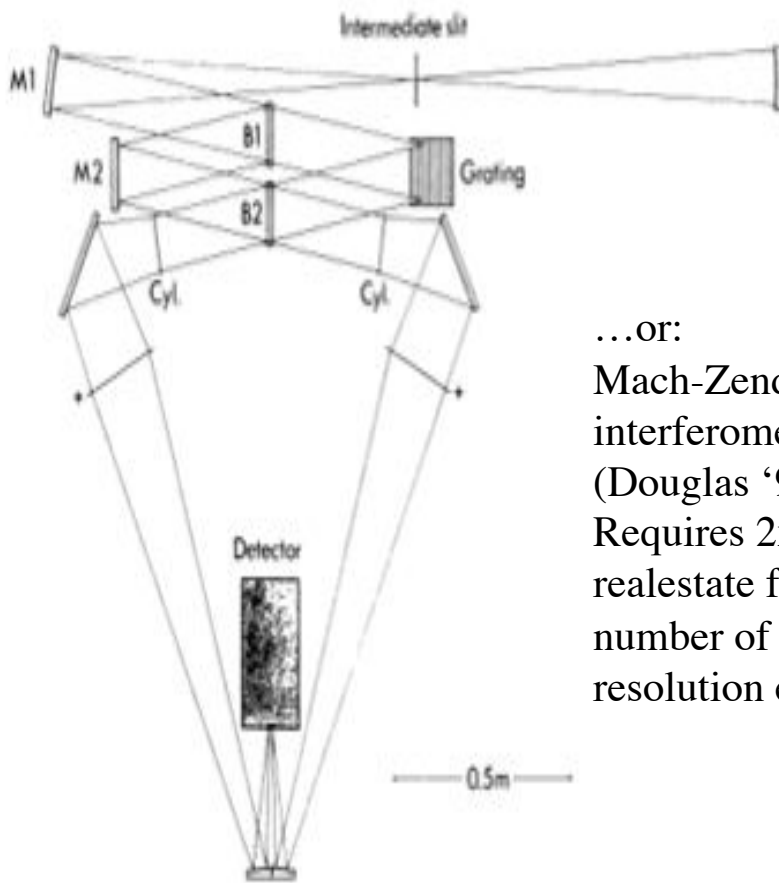


FIG. 4.—Field-widened SHS system. Prisms  $P_1$  and  $P_2$  are chosen so the diffraction gratings appear, from a geometrical optics point of view, coincident and perpendicular to the optical axis.

*Prisms give gratings geometric appearance of being perpendicular to the optical axis.*

# Interferometry-II: Spatial-heterodyne spectroscopy

Standard Michelson and SHS lose half  
the light right from the start:



...or:  
Mach-Zender style  
interferometer  
(Douglas '90).  
Requires 2x detector  
real estate for same  
number of spectral  
resolution elements.

But efficient configurations  
do exist:

*Add prisms for field-widening  
Or gratings for increased R*

*Perfect application for  
holographic grating*

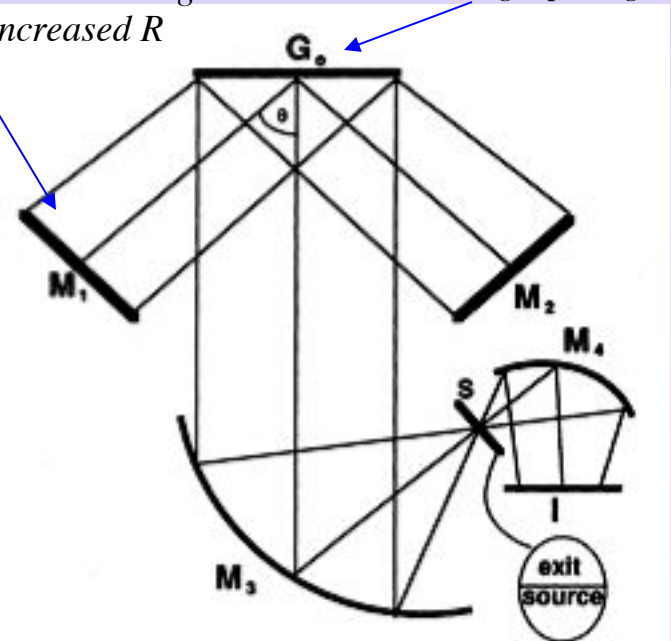


FIG. 5.—Schematic diagram of the all-reflection SHS configuration. Light enters the system through the lower half of split aperture S and exits through the upper half, after which it is imaged by  $M_4$  onto an imaging detector I. The diffraction grating acts as both the beam splitter and dispersive element in the system.

Harlander et al. '92

# Interferometry-II:

## Spatial-heterodyne spectroscopy

- Low-cost, diffraction-limited high-resolution capability  
*but . . .*
- Multiplex disadvantage:
  - $S/N_{\text{SHS}} = S/N_{\text{GS}} * (f/2)^{1/2} (S_{\text{SHS}}/S_{\text{GS}})^{1/2}$ 
    - $S/N_{\text{SHS}}, S/N_{\text{GS}}$  = signal to noise in SHS and grating spectrometer
    - $S_{\text{SHS}}, S_{\text{GS}}$  = total photon signal “
    - $f$  = fraction of total signal in a given spectral channel
      - $f < 1$ , and decreases with bandwidth
  - filter out OH lines (make  $f$  as large as possible)
  - choose small band-width
- Implications for design and use:
  - Make  $f$  as large as possible
    - filter out OH lines (make  $f$  as large as possible)
    - choose small band-width -- but more than Fabry-Perot!

# The detector limit-I:

## Three into two dimensions revisited

